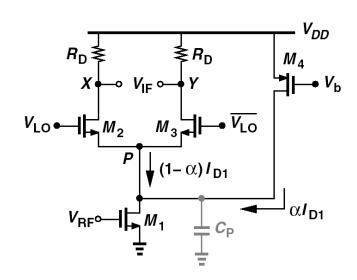
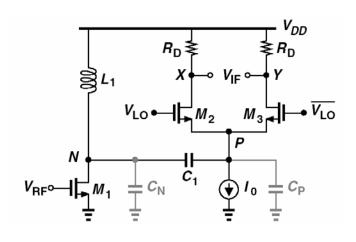
# RF Mixers (III)

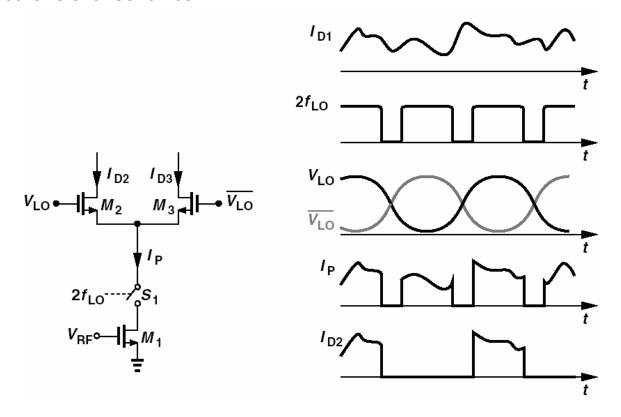
# **Methods of Reducing Flicker Noise in Active Mixers**

Key observation: Reduce I<sub>SS</sub> but without degrading gain, thermal NF, etc.





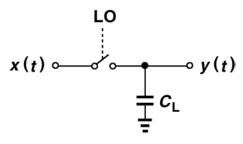
### Or other clever schemes:



[Pullela, ISSCC06]

## **Nonlinearity in Mixers**

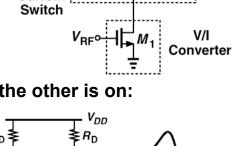
Voltage-driven passive mixers: The LO has a finite transition time, and the on-resistance varies during this time:

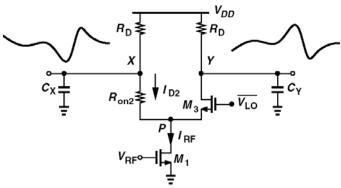


**Active mixers:** 

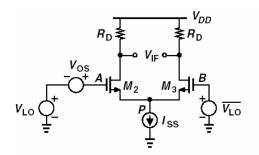
IP3:

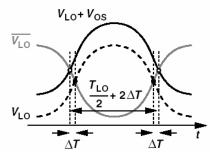
- (1) V/I converter nonlinearity
- (2) When one diff pair device enters triode while the other is on:

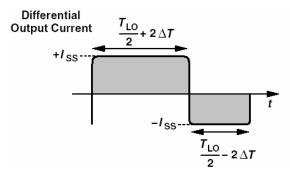




IP2: Asymmetries in the circuit, e.g., between diff pair devices:







#### Observations:

- 1. Should the effect of Vos be similar to that of 1/f noise?
- 2. The differential output current contains a dc term equal to:

$$(4\Delta T/T_{LO})I_{SS} = V_{OS}I_{SS}/(\pi V_{p,LO})$$

3. If we replace Iss with a V/I device and assume two tones, the input transistor generates a beat:

$$V_{RF} = V_m \cos \omega_1 t + V_m \cos \omega_2 t + V_{GS0}$$
$$I_{IM2} = \frac{1}{2} \mu_n C_{ox} \frac{W}{L} V_m^2 \cos(\omega_1 - \omega_2) t$$

4. Need to equate the feedthrough amplitude to the fundamental amplitude:

$$\frac{1}{2}\mu_{n}C_{ox}\frac{W}{L}V_{IIP2}^{2}\frac{V_{OS}R_{D}}{\pi V_{D,LO}} = \frac{2}{\pi}g_{m1}R_{D}V_{IIP2}$$

The IIP2 is thus given by:

For example, if overdrive = 250 mV, LO peak swing = 300 mV, and Vos = 10 mV, then IIP2 = 30 Vp ( $\sim$  40 dBm).

# **Active Mixer Design Example**



Design Specs: 
$$V_{DD} = 1.2 \text{ V}, 65\text{-nm CMOS}, I_{DD} = 2 \text{ mA}, \text{ single-ended LO swing = 400 mV}_{p}$$
Design limited by voltage headroom; Assign:  $V_{DS1} = 300 \text{ mV} \rightarrow W_1 = 15 \text{ um}$ 

$$V_{DS1} = 300 \text{ mV} \rightarrow W_1 = 15 \text{ um}$$

$$g_{m1}$$
= 12.75 ms

$$V_{DS2,3,eq} = 150 \text{ mV} \rightarrow W_{2,3} = 20 \text{ um}$$

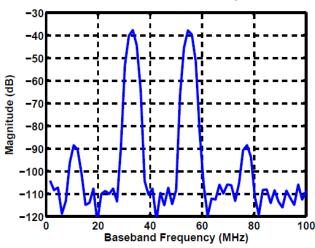
- $\rightarrow$  drop across R<sub>D</sub> = 600 mV
- $\rightarrow$  Choose R<sub>D</sub> = 500 ohms
- Choose  $C_1 = C_2 = 2$  pF to suppress LO feedthrough.

EE215C Win. 13

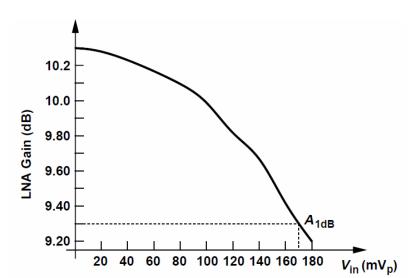
IIP3 Estimate:

Input peak amplitude: 40 mV

B. Razavi HO #2



**Compression Characteristic:** 



**Quick Calculations:** 

• Voltage Conversion Gain:

• Noise Figure:

$$\begin{array}{lcl} \overline{V_{n,in}^2} & = & \pi^2 kT \left( \frac{\gamma}{g_{m1}} + \frac{2}{g_{m1}^2 R_D} \right) \\ & = & 4.21 \times 10^{-18} \ \mathrm{V^2/Hz}, \end{array}$$

 $\implies NF_{SSB} = 1 + \frac{\overline{V_{n,in}^2}}{4kTR_S}$ = 6.1 (= 7.84 dB)

