

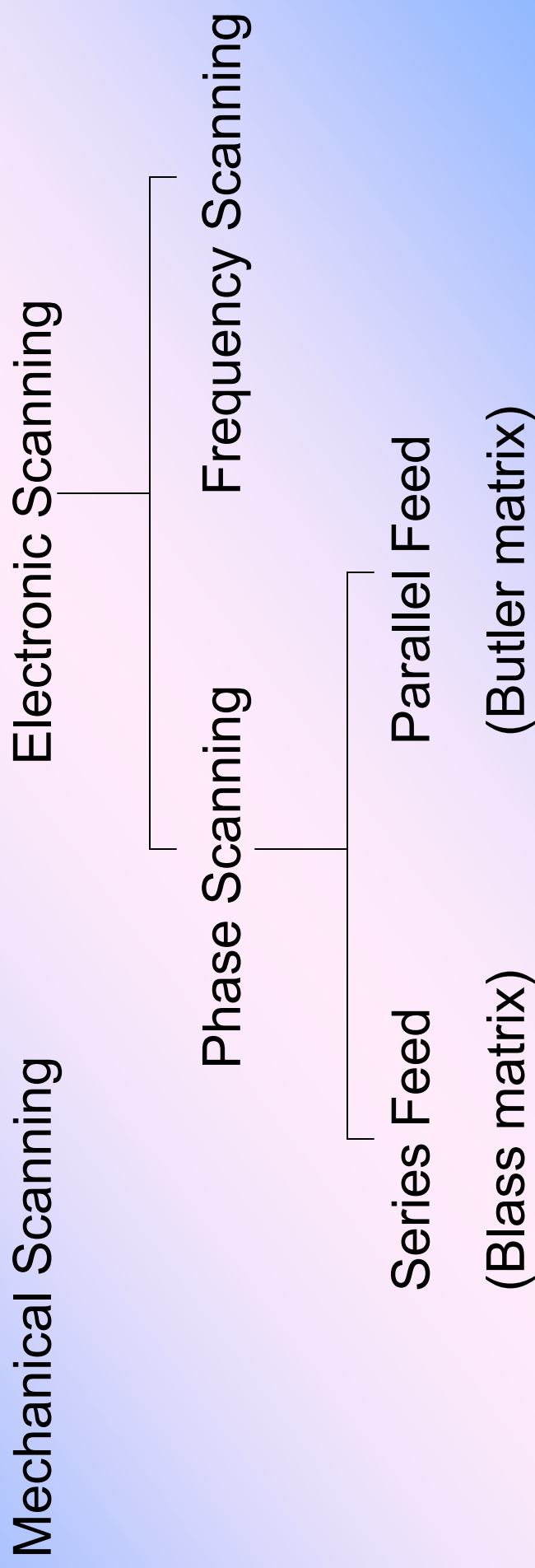
DESIGN AND IMPLEMENTATION OF BUTLER MATRIX

-Simultaneous beam formation

-Harish Rajagopalan

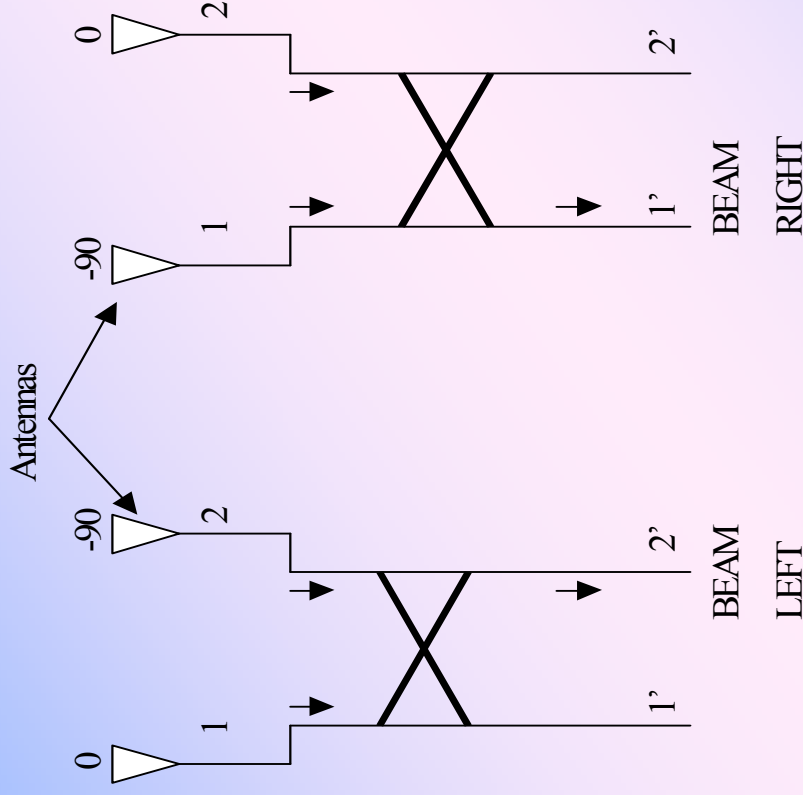
- ☞ Objective
- ☞ Elements of Butler matrix
- ☞ Study of 2x2, 4x4 and 8x8 butler matrices
- ☞ Testing and results for 4x4
- ☞ Conclusion and future scope

Antenna Beam Scanning Methods



Principle of Butler matrix

Incident wavefront



$$I_1 = A_1 e^{j0} \text{ ----- (1)}$$

$$I_2 = A_2 e^{j\pi/2} \text{ ----- (2)}$$

$$\text{and } A_1 = A_2 \text{ ----- (3)}$$

$$I_1' = I_1 + I_2 e^{j\pi/2}$$

$$\text{or } I_1' = A_1 e^{j0} + A_2 e^{j\pi} \text{ ----- (4)}$$

$$I_2' = I_1 e^{j\pi/2} + I_2,$$

$$I_2' = A_1 e^{j\pi/2} + A_2 e^{j\pi/2},$$

$$\text{Or } I_2' = (A_1 + A_2) e^{j\pi/2} \text{ ----- (5)}$$

A_1 and $A_2 \rightarrow$ amplitudes of antenna currents

I_1 and $I_2 \rightarrow$ Input antenna currents I_1' and $I_2' \rightarrow$ output antenna currents

Characteristics of Butler matrix

-Number of beams = Number of antenna elements = N

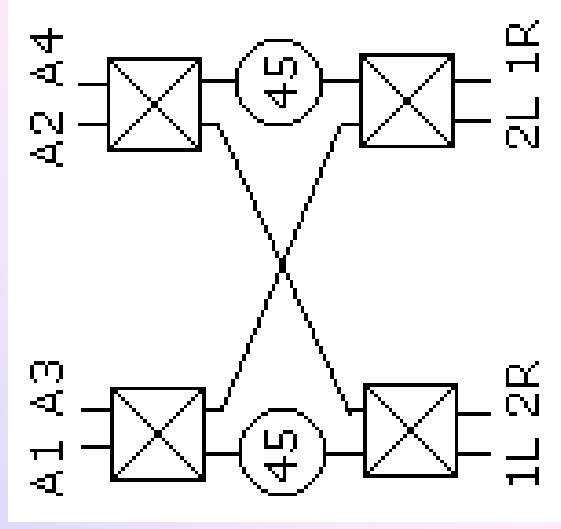
-Number of Hybrid rings = $N/2 \log_2 N$

-Number of Phase shifters = $N/2 (\log_2 N - 1)$

-Low insertion loss

-Uniform antenna array illumination

4 x 4 Butler matrix



$$1L = A1 \angle 45^\circ + A2 \angle 90^\circ + A3 \angle 135^\circ + A4 \angle 180^\circ$$

$$2R = A1 \angle 135^\circ + A2 \angle 0^\circ + A3 \angle 225^\circ + A4 \angle 90^\circ$$

$$2L = A1 \angle 90^\circ + A2 \angle 225^\circ + A3 \angle 0^\circ + A4 \angle 135^\circ$$

$$1R = A1 \angle 180^\circ + A2 \angle 135^\circ + A3 \angle 90^\circ + A4 \angle 45^\circ$$

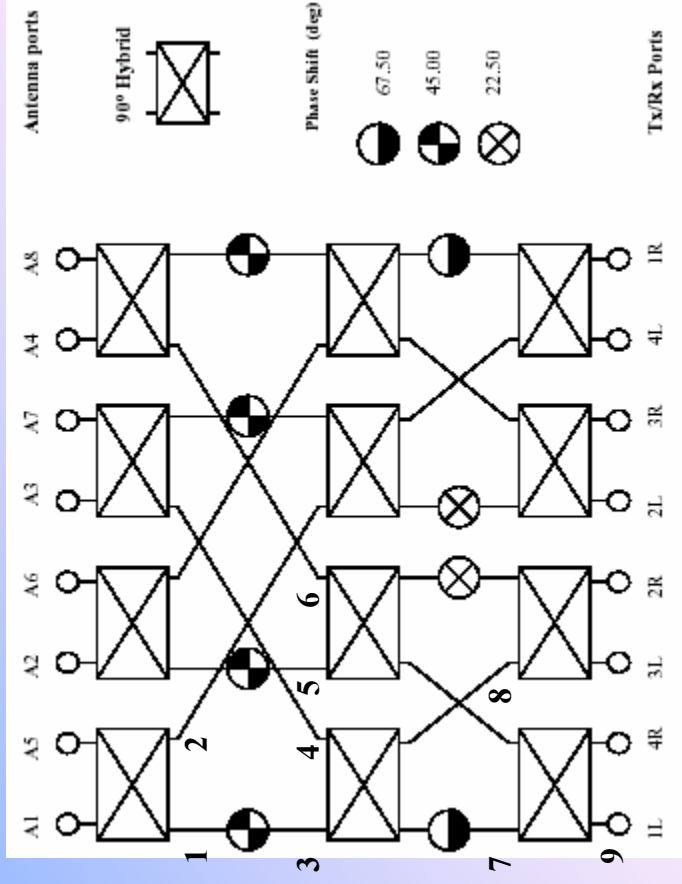
Phase matrix of 4 x 4 Butler matrix

$$\begin{bmatrix} 2R \\ 1R \\ 1L \\ 2L \end{bmatrix} = \begin{bmatrix} e^{-j3/4\pi} & e^{-j0\pi} & e^{-j5/4\pi} & e^{-j\pi/2} \\ e^{-j\pi} & e^{-j3/4\pi} & e^{-j\pi/2} & e^{-j\pi/4} \\ e^{-j\pi/4} & e^{-j\pi/2} & e^{-j3/4\pi} & e^{-j\pi} \\ e^{-j\pi/2} & e^{-j5/4\pi} & e^{-j0\pi} & e^{-j3/4\pi} \end{bmatrix} \begin{bmatrix} A_1 \\ A_2 \\ A_3 \\ A_4 \end{bmatrix}$$

$$\begin{bmatrix} 2R \\ 1R \\ 1L \\ 2L \end{bmatrix} = \begin{bmatrix} 0 & -135 & 90 & -45 \\ 0 & -45 & -90 & -135 \\ 0 & 45 & 90 & 135 \\ 0 & 135 & -90 & 45 \end{bmatrix} \begin{bmatrix} A_1 \\ A_2 \\ A_3 \\ A_4 \end{bmatrix}$$

Phase progression

8 x 8 Butler matrix



Equation for 1L port.

At point 1: $A1 + A5 \angle 90$

At point 2: $A2 + A6 \angle 90$

At point 3: $A1 \angle 45 + A5 \angle 135$

At point 4: $A3 + A7 \angle 90$

At point 5: $A2 \angle 45 + A6 \angle 135$

At point 6: $A4 + A8 \angle 90$

At point 7: $A1 \angle 45 + A5 \angle 90 + A3 \angle 90$
 $+ A7 \angle 180$

At point 8: $A2 \angle 45 + A6 \angle 135 + A4 \angle 90$
 $+ A8 \angle 180$

At point 9: $A1 \angle 112.5 + A5 \angle 157.5$
 $+ A3 \angle 157.5 + A7 \angle 247.5$

At port 1L: $A1 \angle 112.5 + A3 \angle 157.5 + A7 \angle 247.5 + A2 \angle 135 + A6 \angle 225 + A4 \angle 180 + A8 \angle 270$

Phase matrix of 8 x 8 Butler matrix

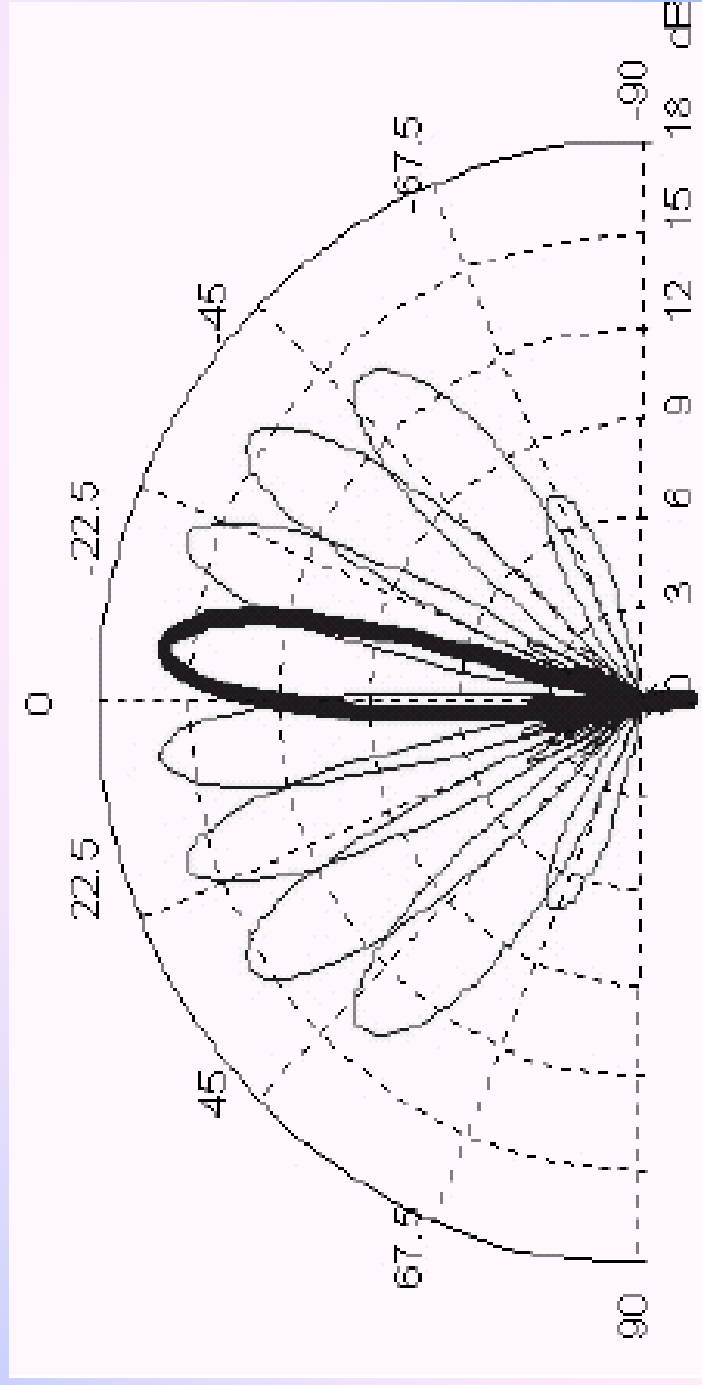
$$\begin{bmatrix} 4R \\ 3R \\ 2R \\ 1R \\ 1L \\ 2L \\ 3L \\ 4L \end{bmatrix} = \begin{bmatrix} e^{-j9\frac{\pi}{8}} & e^{-j2\frac{\pi}{8}} & e^{-j11\frac{\pi}{8}} & e^{-j4\frac{\pi}{8}} & e^{-j13\frac{\pi}{8}} & e^{-j6\frac{\pi}{8}} & e^{-j15\frac{\pi}{8}} & e^{-j8\frac{\pi}{8}} \\ e^{-j9\frac{\pi}{8}} & e^{-j4\frac{\pi}{8}} & e^{-j15\frac{\pi}{8}} & e^{-j10\frac{\pi}{8}} & e^{-j5\frac{\pi}{8}} & e^0 & e^{-j11\frac{\pi}{8}} & e^{-j6\frac{\pi}{8}} \\ e^{-j10\frac{\pi}{8}} & e^{-j7\frac{\pi}{8}} & e^{-j4\frac{\pi}{8}} & e^{-j\frac{\pi}{8}} & e^{-j14\frac{\pi}{8}} & e^{-j8\frac{\pi}{8}} & e^{-j5\frac{\pi}{8}} & e^{-j1\frac{\pi}{8}} \\ e^{-j12\frac{\pi}{8}} & e^{-j11\frac{\pi}{8}} & e^{-j10\frac{\pi}{8}} & e^{-j9\frac{\pi}{8}} & e^{-j8\frac{\pi}{8}} & e^{-j7\frac{\pi}{8}} & e^{-j6\frac{\pi}{8}} & e^{-j5\frac{\pi}{8}} \\ e^{-j5\frac{\pi}{8}} & e^{-j6\frac{\pi}{8}} & e^{-j7\frac{\pi}{8}} & e^{-j8\frac{\pi}{8}} & e^{-j9\frac{\pi}{8}} & e^{-j10\frac{\pi}{8}} & e^{-j11\frac{\pi}{8}} & e^{-j12\frac{\pi}{8}} \\ e^{-j5\frac{\pi}{8}} & e^{-j8\frac{\pi}{8}} & e^{-j11\frac{\pi}{8}} & e^{-j14\frac{\pi}{8}} & e^{-j\frac{\pi}{8}} & e^{-j4\frac{\pi}{8}} & e^{-j7\frac{\pi}{8}} & e^{-j10\frac{\pi}{8}} \\ e^{-j6\frac{\pi}{8}} & e^{-j11\frac{\pi}{8}} & e^{-j16\frac{\pi}{8}} & e^{-j5\frac{\pi}{8}} & e^{-j10\frac{\pi}{8}} & e^{-j15\frac{\pi}{8}} & e^{-j4\frac{\pi}{8}} & e^{-j9\frac{\pi}{8}} \\ e^{-j8\frac{\pi}{8}} & e^{-j15\frac{\pi}{8}} & e^{-j6\frac{\pi}{8}} & e^{-j13\frac{\pi}{8}} & e^{-j4\frac{\pi}{8}} & e^{-j11\frac{\pi}{8}} & e^{-j2\frac{\pi}{8}} & e^{-j9\frac{\pi}{8}} \end{bmatrix} \cdot \begin{bmatrix} A_1 \\ A_2 \\ A_3 \\ A_4 \\ A_5 \\ A_6 \\ A_7 \\ A_8 \end{bmatrix}$$

Phase progression

	Antenna Ports							
	1	2	3	4	5	6	7	8
4R	0	157.5	315	112.5	270	67.5	225	22.5
3R	0	112.5	225	337.5	90	202.5	315	67.5
2R	0	67.5	135	202.5	270	337.5	45	12.5
1R	0	22.5	45	67.5	90	112.5	135	157.5
1L	0	-22.5	-45	-67.5	-90	-112.5	-135	-157.5
2L	0	-67.5	-135	-202.5	-270	-337.5	-45	-12.5
3L	0	-112.5	-225	-337.5	-90	-202.5	-315	-67.5
4L	0	-157.5	-315	-112.5	-270	-67.5	-225	-22.5

Values are degrees

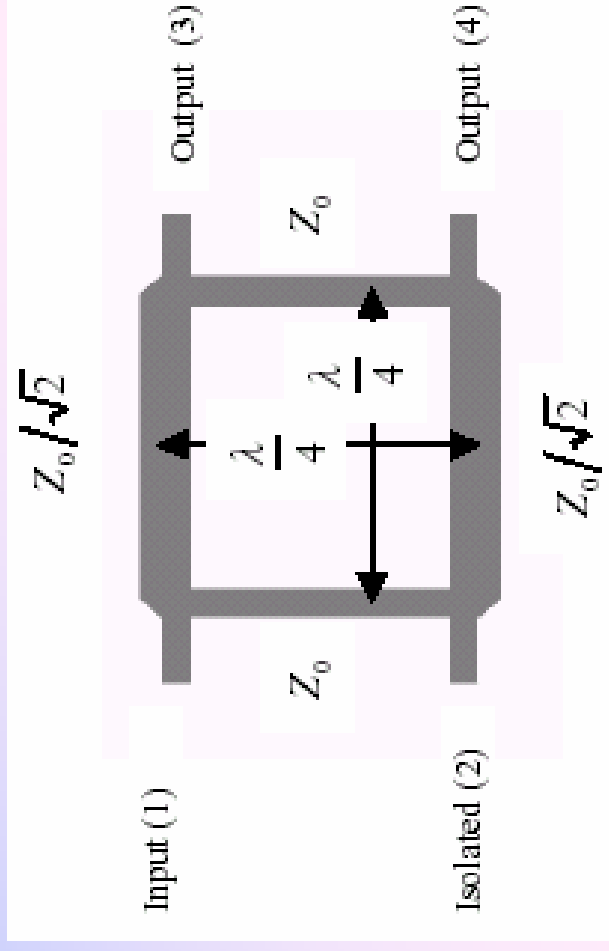
Beam pattern for 8x8 Butler matrix



Components of Butler matrix

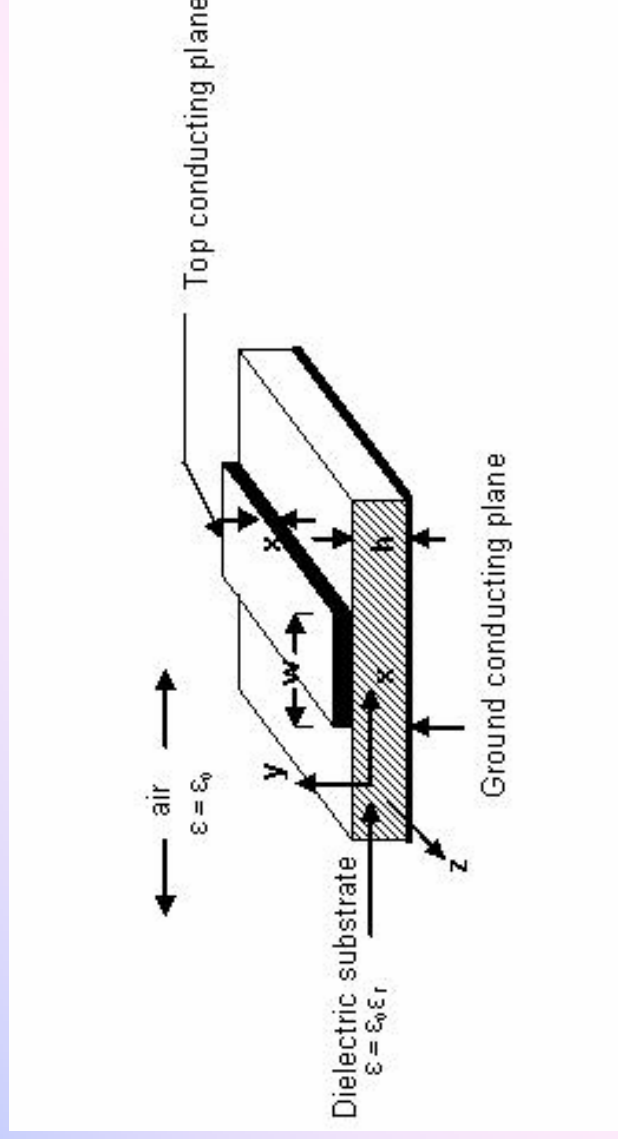
- Quadrature hybrid
- Fixed phase shifter
- Helical antenna

Quadrature Hybrid



Branch line coupler

Microstrip Lines



Basic Structure

Design Of Hybrid (Branchline Coupler)

Frequency = 1 GHz

Wavelength (in air) = 30 cm.

Substrate used for PCB manufacturing is FR-4 Glass Epoxy.

For FR-4 board, Relative dielectric constant (ϵ_r) = 4.4

The height of the dielectric (d) = 1.6 mm

Characteristic impedance $Z_0 = 50 \Omega$

$$Z_{o1} = Z_0 \sqrt{2} = 35.35 \Omega$$

Formulae:

1. Effective Dielectric constant(ϵ_e) = $\frac{\epsilon_r + 1}{2} + \frac{\epsilon_r - 1}{2} \frac{d}{W}$
2. $W/d = \frac{2}{\pi} [B - 1 - \ln(2B - 1) + (\epsilon_r - 1)/2\epsilon_r \{ \ln(B - 1) + 0.39 - 0.61/\epsilon_r \}]$ $W/d > 2$

where

$$B = \frac{377\pi}{2Z_0(\epsilon_r)^{1/2}}$$

$$2Z_0(\epsilon_r)^{1/2}$$

Calculations

For 50Ω

$$B = 5.646312$$

$$W/d = 1.91335$$

$$W = 3.06136 \text{ mm}$$

$$\epsilon_{\text{eff}} = 3.33024$$

$$\lambda_{\text{microstrip}} = \lambda_0 / \sqrt{\epsilon_{\text{eff}}} = 16.43886 \text{ cm}$$

$$\text{Length of track} = \lambda_{\text{microstrip}}/4 = 4.1097 \text{ cm}$$

For 35.35Ω

$$B = 7.98629$$

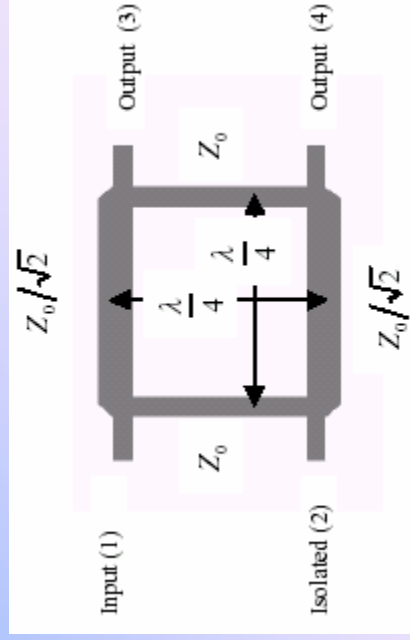
$$W/d = 3.26475$$

$$W = 5.2236$$

$$\epsilon_{\text{eff}} = 3.48619$$

$$\lambda_{\text{microstrip}} = \lambda_0 / \sqrt{\epsilon_{\text{eff}}} = 16.0674 \text{ cm}$$

$$\text{Length of track} = \lambda_{\text{microstrip}}/4 = 4.0168 \text{ cm}$$



Fixed Phase shifter

- **Outer Conductor (Copper)**
 - minimizes the power loss
 - maximizes the mechanical integrity
 - provides the desired interface with connections
- **Center conductor(Silver plated copper)**
 - acts as primary signal carrier
 - provides excellent high frequency conductivity



Semi rigid cable

- **Dielectric material (Polytetrafluoroethylene)**
 - maintains the spacing and geometry of the cable
 - assures mechanical integrity during forming and bending or under pressure

Design of phase shifter

L1 provides phase shift of a_1°

L2 provides phase shift of a_2°

(L1-L2) provides phase shift of $(a_1-a_2)^\circ$

L1 \rightarrow a1

L1 = 10 cm, $a_1 = 97.2^\circ$

L2 = 15 cm, $a_2 = 18.5^\circ$

$(15-10)$ cm $\rightarrow (18.5-97.2)^\circ$

5 cm $\rightarrow -78.7^\circ$

1 cm $\rightarrow -15.7^\circ$

22.87 cm $\rightarrow 360^\circ$

L2 \rightarrow a2

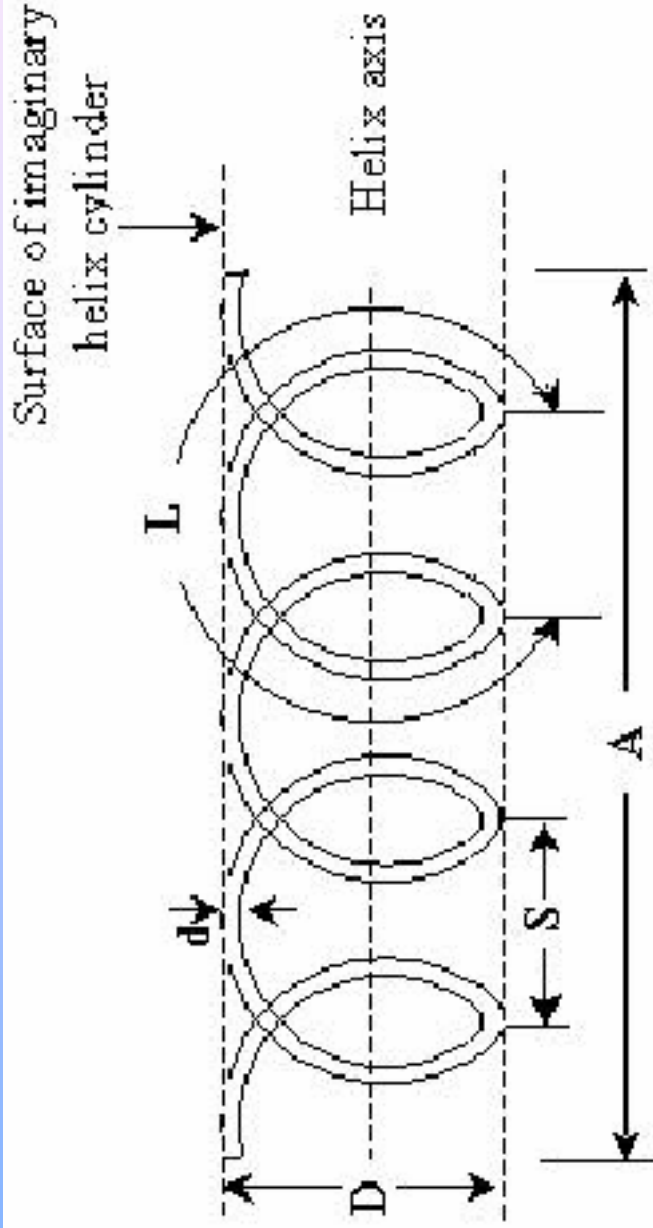
λ_c - wavelength in cable = 22.8 cm

λ_a - wavelength in air = 30.0 cm

Velocity factor = $\lambda_c/\lambda_a = 76\%$.

Differential measurement

Helical antenna



$$D = 110 \text{ mm}$$

$$d = 2 \text{ mm}$$

$$L = 353.5 \text{ mm}$$

$$S = 75 \text{ mm}$$

$$A = 450 \text{ mm}$$

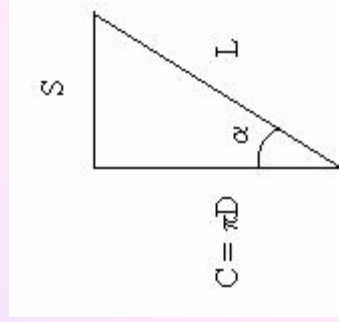
$$C = \pi D = 345.5 \text{ mm}$$

$$\alpha = \arctan S/\pi D = 12.24^\circ$$

N = number of turns = 6

$$1.2 \geq C_\lambda \geq 0.8,$$

$$14^\circ \geq \alpha \geq 12^\circ \text{ and } n \geq 4$$



Helical geometry

Transmission And Radiation Modes Of Helix

1. Normal mode-

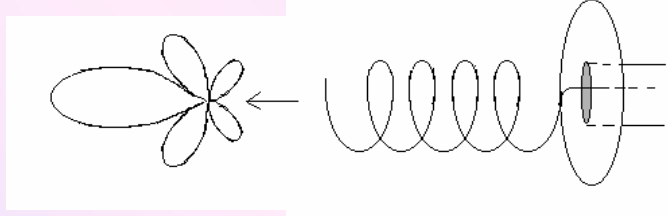
The field radiated by the antenna is maximum in a plane normal to the helix and minimum along its axis.

2. Axial mode

The field radiated by the antenna is maximum along its axis.

Power Beam Width (HPBW) = $\underline{52} = 36^\circ$

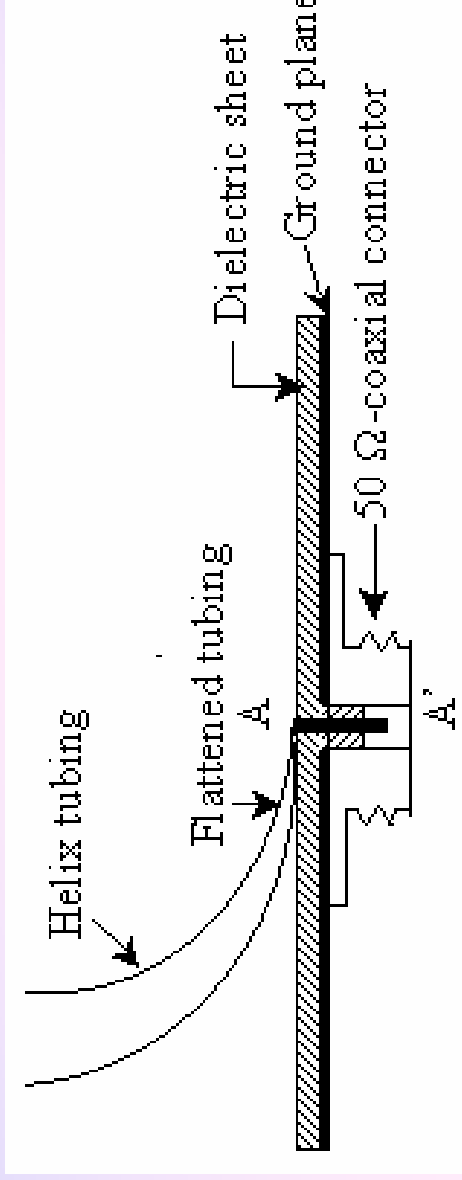
$$c\lambda\sqrt{ns\lambda}$$



Impedance matching

With axial feed the terminal impedance (resistive) is given by

$$R = 140C\lambda \quad (\Omega)$$



Gradually tapered transition from helix to coaxial line

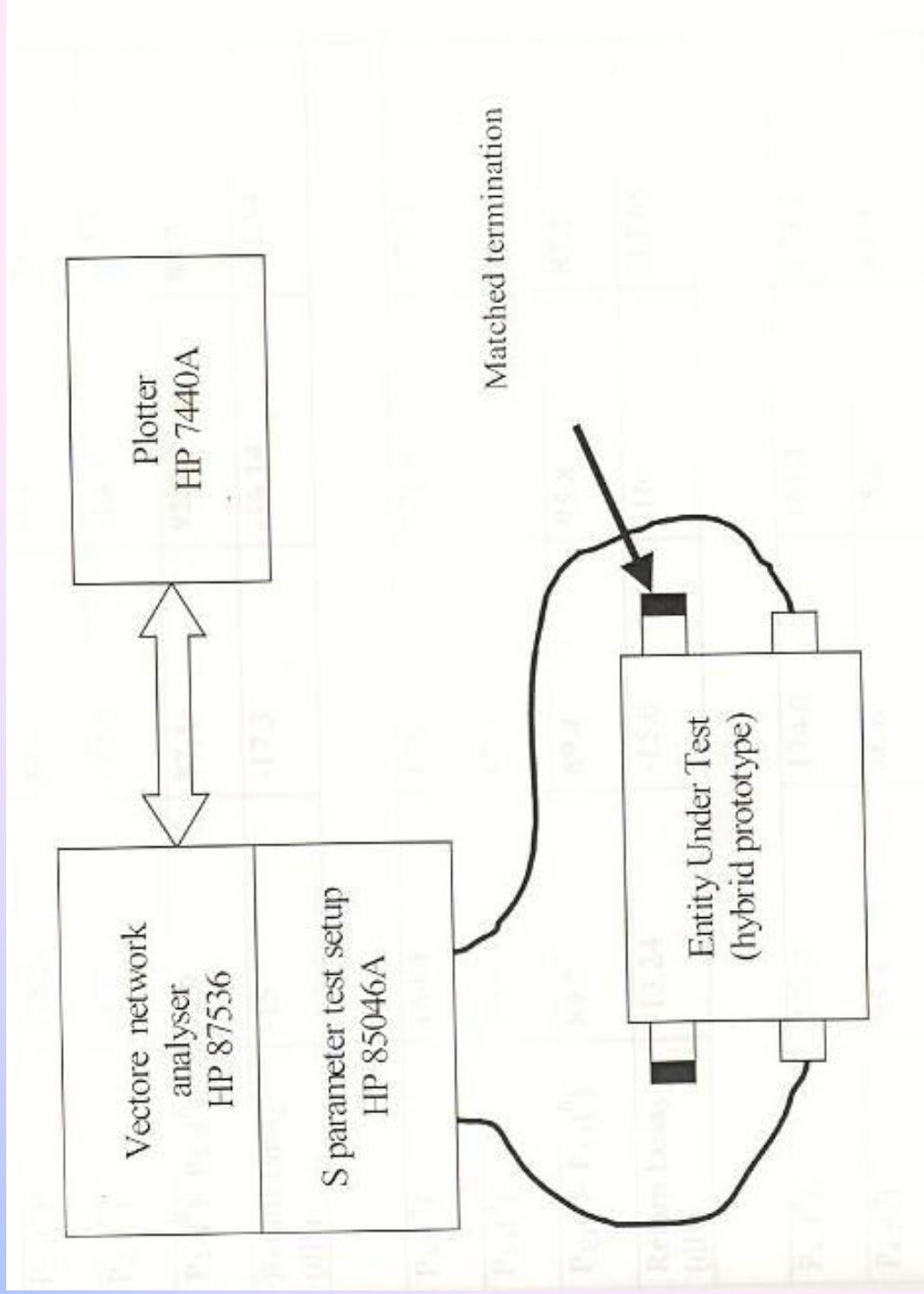
Testing and Results

Testing of Phase shifter

Testing of 4 x 4 Butler matrix

Beam formation of 4 x 4 Butler matrix

Testing of Hybrid



TESTING OF HYBRIDS ON ONE CARD:

Ports	Hybrid A	Hybrid B	Hybrid C	Hybrid D
$P_{1/4}(\text{C})$	-116.6	175.4	161.5	177
$P_{1/3}(\text{C})$	151.8	84.9	73.7	86.6
$P_{1/4}(\text{C}) - P_{1/3}(\text{C})$	91.6	90.5	87.8	90.4
Return Loss ₁ (dB)	-16.2	-17.48	-15.6	-16.16
The Loss of the several hybrids used was in the range 1.5 - 2 dB.				
$P_{2/4}(\text{C})$	178.5	84.9	75.9	78.8
$P_{2/3}(\text{C})$	85.6	172.3	168.7	167.5
$P_{2/4}(\text{C}) - P_{2/3}(\text{C})$	92.9	87.4	92.8	88.7
Return Loss ₂ (dB)	-15	-17.3	-16.14	-12.54
.				
$P_{3/2}(\text{C})$	169.4	176.7	171.8	171.3
$P_{3/1}(\text{C})$	79.7	87.3	76	84.1
$P_{3/2}(\text{C}) - P_{3/1}(\text{C})$	89.7	89.4	95.8	87.2
Return Loss ₃ (dB)	-13.24	-15.6	-16	-13.65
.				
$P_{4/1}(\text{C})$	171.7	174.0	161.1	174.4
$P_{4/2}(\text{C})$	85.8	86.6	75.6	83.9
$P_{4/1}(\text{C}) - P_{4/2}(\text{C})$	85.9	87.4	85.5	90.5
Return Loss ₄ (dB)	-15.23	-16.42	-14.2	-17.24

READINGS FOR 4x4 BUTLER MATRIX

THEORETICAL MATRIX

$$\begin{bmatrix} 2R \\ 1R \\ 1L \\ 2L \end{bmatrix} = \begin{bmatrix} 135 & 0 & 225 & 90 \\ 180 & 135 & 90 & 45 \\ 45 & 90 & 135 & 180 \\ 90 & 225 & 0 & 135 \end{bmatrix} * \begin{bmatrix} A_1 \\ A_2 \\ A_3 \\ A_4 \end{bmatrix}$$

THEORETICAL PROGRESSIVE PHASE SHIFT

$$\begin{bmatrix} 2R \\ 1R \\ 1L \\ 2L \end{bmatrix} = \begin{bmatrix} 0 & -135 & 90 & -45 \\ 0 & -45 & -90 & -135 \\ 0 & 45 & 90 & 135 \\ 0 & 135 & -90 & 45 \end{bmatrix} * \begin{bmatrix} A_1 \\ A_2 \\ A_3 \\ A_4 \end{bmatrix}$$

OBSERVED READINGS

$$\begin{bmatrix} 2R \\ 1R \\ 1L \\ 2L \end{bmatrix} = \begin{bmatrix} 77.5 & -155.3 & -12.3 & 109.5 \\ 32.5 & 65.3 & 118.7 & 157.8 \\ 170.8 & 116.2 & 81.4 & 64.1 \\ 125.4 & -21.6 & -144.8 & 64.1 \end{bmatrix} * \begin{bmatrix} A_1 \\ A_2 \\ A_3 \\ A_4 \end{bmatrix}$$

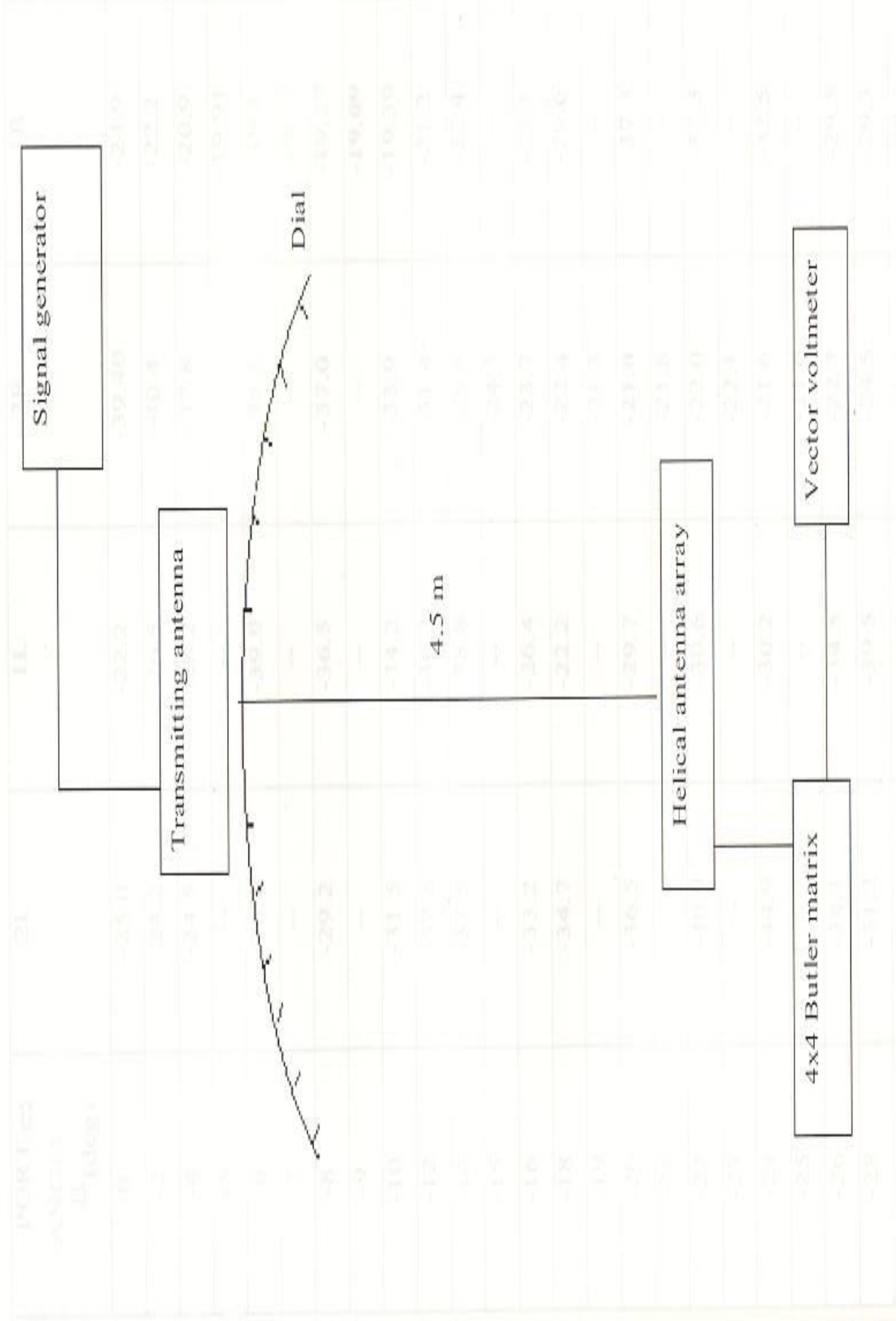
$$\begin{bmatrix} 2R \\ 1R \\ 1L \\ 2L \end{bmatrix} = \begin{bmatrix} 0 & 127.2 & -89.8 & 32 \\ 0 & 33 & 86.4 & 119.5 \\ 0 & -54.6 & -89.4 & -148.3 \\ 0 & -147 & 89.8 & -61.3 \end{bmatrix} * \begin{bmatrix} A_1 \\ A_2 \\ A_3 \\ A_4 \end{bmatrix}$$

SETUP FOR BEAM PATTERN OF 4X4 BUTLER MATRIX:

Input Frequency = 1 GHz

Input Power = 13dBm

Output power in dBm



TESTING FOR 4X4 BUTLER MATRIX:

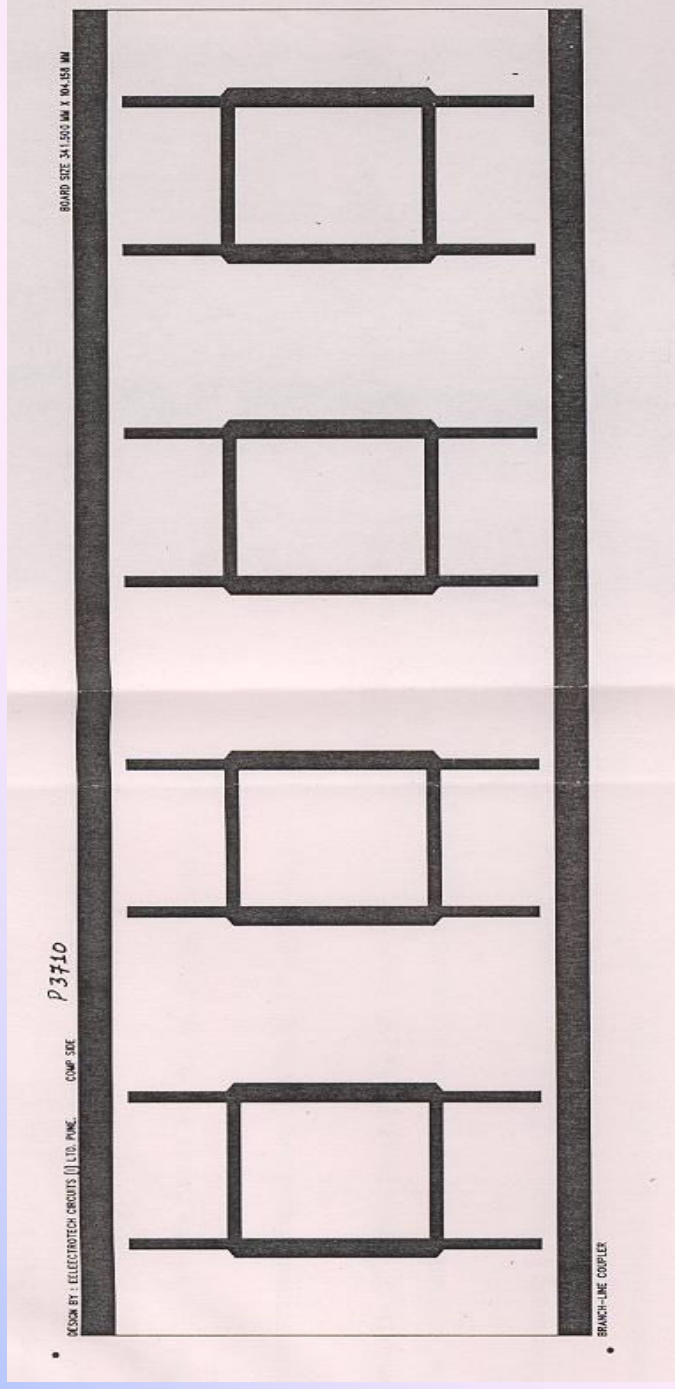
Input Frequency = 1 GHz

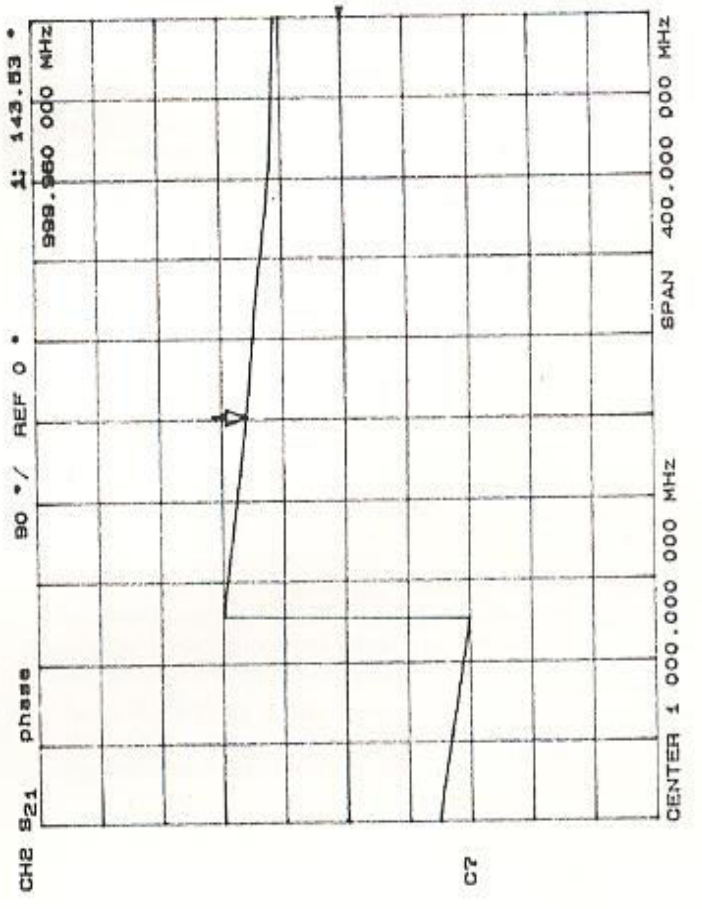
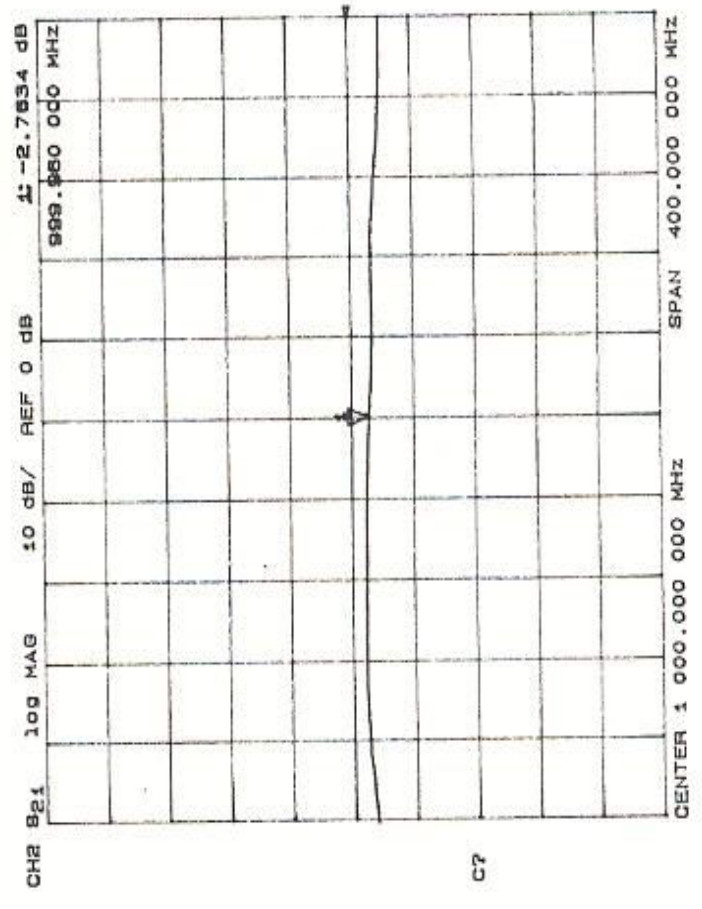
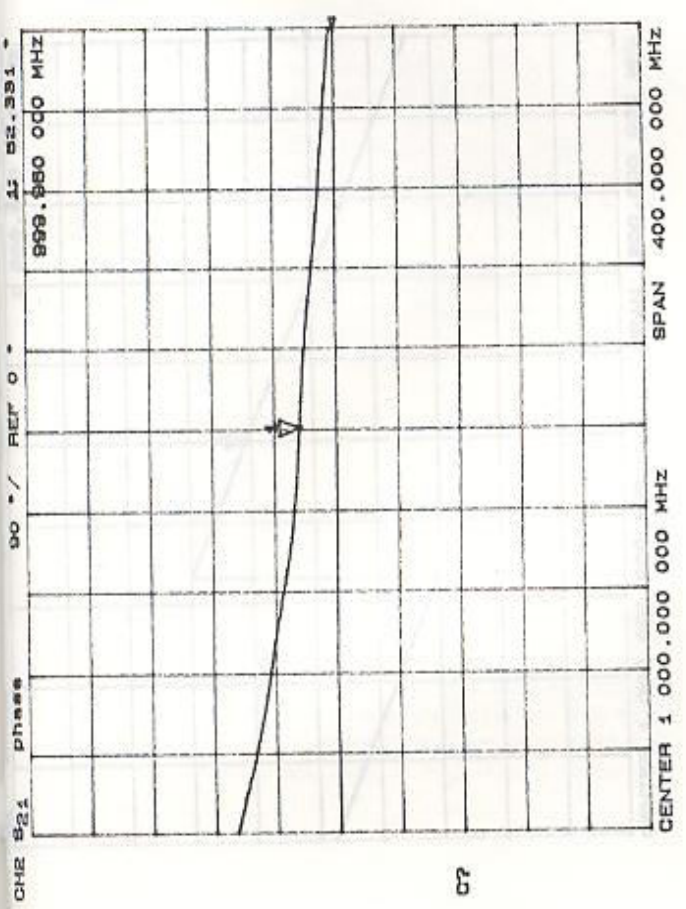
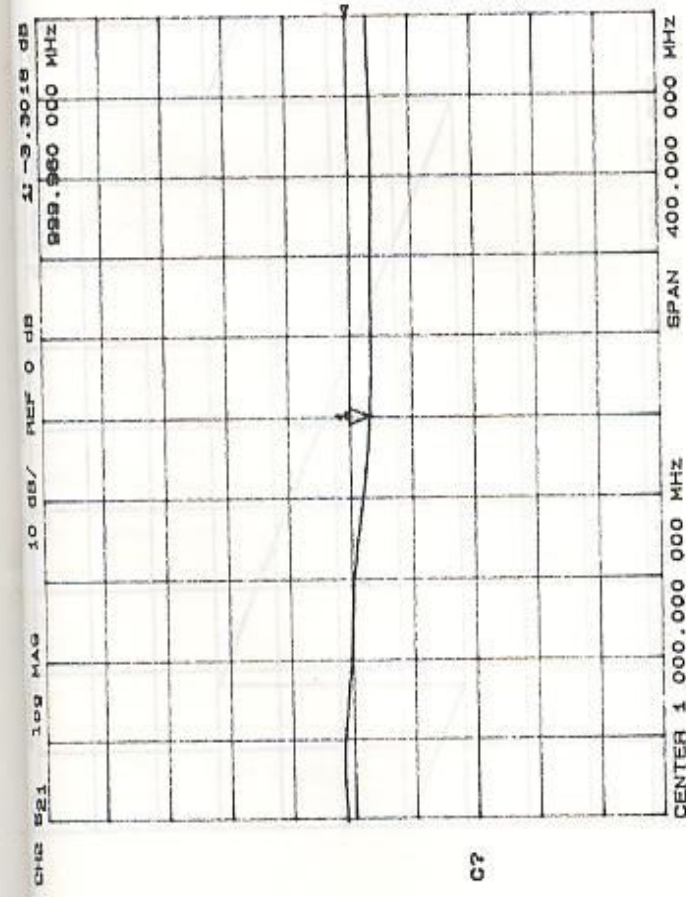
Input Power = +13dBm Output power in dBm

PORT \Rightarrow ANGLE Γ (deg)	2L	1L	2R	1R
0	-25.0	-22.2	-39.40	-24.9
-2	-24.2	-26.5	-40.4	-22.2
-4	-24.5	-28.2	-37.8	-20.9
-5	--	--	--	-19.91
-6	-26.6	-39.9	-38.2	-19.3
-7	--	--	--	-19.33
-8	-29.2	-36.5	-37.0	-19.27
-9	--	--	--	-19.09
-10	-31.5	-34.2	-33.9	-19.39
-12	-32.8	-30.2	-31.4	-21.2
-14	-37.5	-38.8	-28.8	-22.4
-15	--	--	-24.3	--
-16	-33.2	-26.4	-23.7	-25.1
-18	-34.7	-22.2	-22.4	-29.6
-19	--	--	-21.3	--
-20	-36.5	-29.7	-21.0	-37.3
-21	--	--	-21.8	--
-22	-40.9	-30.6	-22.0	-37.3
-23	--	--	-22.1	--
-24	-44.9	-30.2	-21.6	-32.5
-25	--	--	-21.6	--
-26	-34.1	-34.5	-22.7	-29.5
-28	-31.2	-39.5	-24.5	-29.3
-30	-28.9	-43.7	-26.3	-28.3
-32	-28.4	-44.7	-30.0	-29.5

-34	-26.6	-37.9	-33.0	-30.6
2	-27.5	-20.5	-48.2	-30.1
4	-31.2	-19.5	-32.7	-31.6
5	--	-20.5	--	--
6	-40.2	-20.7	-29.9	-31.5
7	--	-20.6	--	--
8	-33.9	-20.9	-28.6	-32.4
9	--	-21.6	--	--
10	-29.7	-22.4	-26.2	-33.3
11	-26.3	--	--	--
12	-23.7	-23.8	-25.5	-35.7
14	-23.5	-25.7	-27.1	-35.2
16	-22.4	-27.4	-26.9	-37.5
18	-22.2	-30.6	-32.9	-36.0
20	-22.6	-35.2	-37.4	-33.2
21	-23.2	--	--	--
22	-22.5	-36.4	-42.1	-29.7
23	-23.2	--	--	--
24	-24.5	-36.7	-36.2	-28.3
26	-26.2	-37.2	-32.4	-29.3
28	-29.4	-40.3	-28.4	-29.4
30	-30.2	-38.5	-28.0	-30.5
32	-32.7	-34.8	-26.8	-33.4
34	-34.2	-33.5	-26.6	-36.1

PCB Layout





Applications

- tracking of radio sources**
- direction finding**

Future scope

- Adaptive array and smart antenna**
- Digitization**

LIST OF REFERENCES:

- [1] Y. T. Lo and S. W. Lee, Antenna handbook, theory, applications and design, Van Nostrand Reinhold company, New York, 1988.
- [2] Richard C. Johnson and Henry Jasik, Antenna Engineering Handbook, 2nd edition, McGraw Hill book company, New york, 1961.
- [3] Constantine A. Balanis, Antenna theory, analysis and design, Harper and Row publishers, New York, 1981.
- [4] Richard C. Johnson, Antenna Engineering Handbook, 3rd edition, McGraw Hill book company Inc.
- [5] John D. Kraus, Antennas, 2nd edition, Tata McGraw Hill, 1997.
- [6] R. C. Hansen, Microwave scanning antennas, VOL III, Education Academic Press Inc.-1969.
- [7] David M. Pozer, Microwave Engineering, 2nd Edition, John Wiley & Sons Inc. 1998.
- [8] Vijay Jain, Project report on branch line coupler at ISRO, 1991

THANK YOU