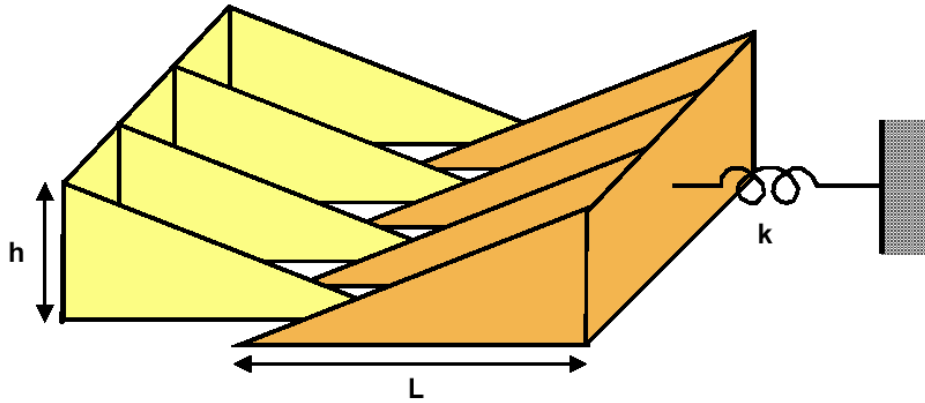


**EE M250B / MAE M282 / BME M250B
HW#3 Solution**



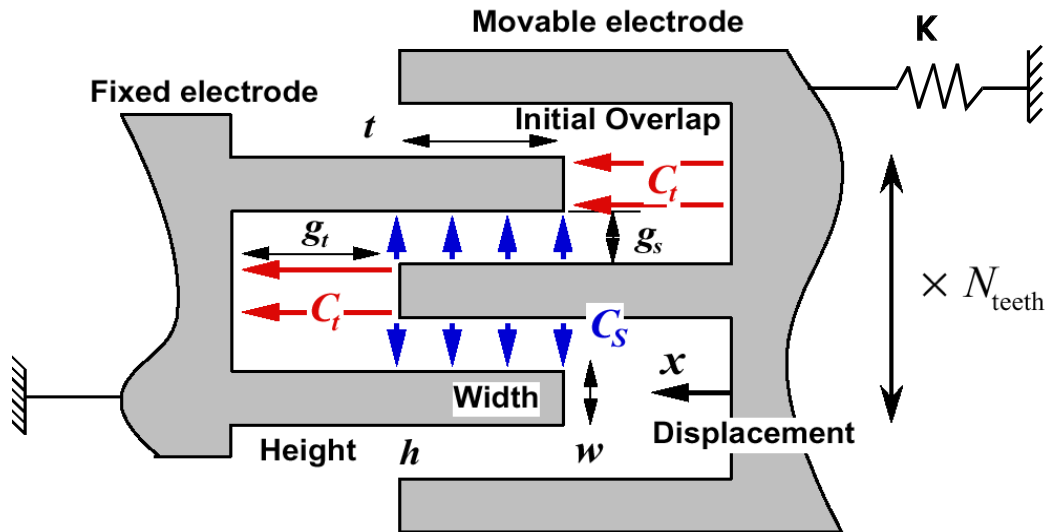
(a)

Given: $\tan\theta = h/L$

Assume that

- (1) the initial overlap length: t
- (2) the displacement of the movable comb: x
- (3) we can neglect the fringe field.

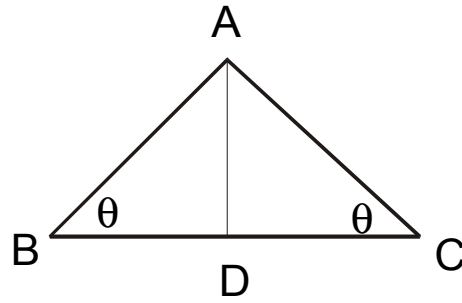
For the schematic view of the comb drive shown below:



The capacitance between the finger's tips: $C_t \approx 0$

The capacitance between the sides of the fingers: $C_s = 2 \frac{\epsilon_0 A}{g}$

For a given displacement x , the overlap area is the triangle as shown below:



Where

$$\overline{BC} = t + x$$

$$\overline{AD} = \frac{1}{2} \overline{BC} \tan \theta = \frac{h}{2L} (t + x)$$

Overlap area

$$A = \frac{1}{2} \overline{BC} \times \overline{AD} = \frac{h}{4L} (t + x)^2$$

Therefore, we can get C_s :

$$C_s = 2 \frac{\epsilon_0}{g} \left(\frac{h}{4L} \right) (t + x)^2 = \frac{\epsilon_0 h}{2gL} (t + x)^2$$

Total capacitance of N gaps C :

$$C = N \times C_s = \frac{\epsilon_0 h N}{2gL} (t + x)^2$$

So, the electrostatic energy stored in the triangular comb drive is:

$$W^* = \frac{1}{2} C V^2 = \frac{\epsilon_0 h N}{4gL} V^2 (t + x)^2$$

(b) The electrostatic force: (in x -direction)

$$F_e = \frac{\partial W^*}{\partial x} = \frac{1}{2} V^2 \frac{\partial C}{\partial x} = \frac{1}{2} V^2 \frac{\partial}{\partial x} \left[\frac{\epsilon_0 h N}{2gL} (t + x)^2 \right] = V^2 \left(\frac{\epsilon_0 h N}{2gL} \right) (t + x)$$

(c)

$$F_{\text{net}} = F_e - F_m = V^2 \left(\frac{\epsilon_0 h N}{2gL} \right) (t + x) - kx,$$

For small perturbation δx ,

$$\delta F_{\text{net}} = \left(\frac{\partial F_{\text{net}}}{\partial x} \right)_V \delta x = \left(V^2 \times \frac{\epsilon_0 h N}{2gL} - k \right) \delta x$$

When

$$\left(V^2 \times \frac{\epsilon_0 h N}{2gL} - k \right) \leq 0 \quad \implies \text{Stable}$$

$$\text{That is, } V^2 \leq \frac{2gLk}{\epsilon_0 h N}, \quad \text{or } V \leq \sqrt{\frac{2gLk}{\epsilon_0 h N}} = V_{\text{PI}}.$$

So, for the triangular comb drive, we will have pull-in if $V > \sqrt{\frac{2gLk}{\epsilon_0 h N}}$,

(d)

Electrostatic force of N fingers:

$$F_e = V^2 \times \left(\frac{\epsilon_0 h N}{2gL} \right) (t + x)$$

Mechanical spring force:

$$F_m = kx$$

For equilibrium: $F_e = F_m$, we can get:

$$V^2 \times \left(\frac{\epsilon_0 h N}{2gL} \right) (t + x) = kx$$

The transfer function of displacement and driving voltage is:

$$x = \frac{V^2 \left(\frac{\epsilon_0 h N t}{2gL} \right)}{k - V^2 \left(\frac{\epsilon_0 h N t}{2gL} \right)}$$

(e)

For a poly-Si folded beam:

$$w_s = 2\mu\text{m}, \quad t_s = 2\mu\text{m}, \quad l_s = 100\mu\text{m}, \quad E = 160\text{GPa}$$

The spring constant of the pair of folded springs is:

$$k = 2 \times \frac{6EI}{l_s^3} = \frac{E w_s t_s^3}{l_s^3} = \frac{160 \times 10^9 \times 2 \times 10^{-6} \times (2 \times 10^{-6})^3}{(100 \times 10^{-6})^3} = 2.56 \text{ N/m}$$

(f)

For $h = 10\mu\text{m}$, $L=50\mu\text{m}$, $g=2\mu\text{m}$, $V=20$ volt, $k=1.28$ N/m
assume that $N=100$ and initial overlap $t= 10\mu\text{m}$

Plug into the equation from (d)

$$V^2 = \frac{2gLkx}{\epsilon_0 h N (t+x)}$$

$$20^2 = \frac{2 \times 2 \times 10^{-6} \times 50 \times 10^{-6} \times 1.28 \times x \times 10^{-6}}{8.85 \times 10^{-12} \times 10 \times 10^{-6} \times 100 \times (10 \times 10^{-6} + x \times 10^{-6})}$$

displacement : $x=0.14 \mu\text{m}$

actuating force: $F = kx = 1.28 \times 0.14 \times 10^{-6} = 1.79 \times 10^{-7}$ N