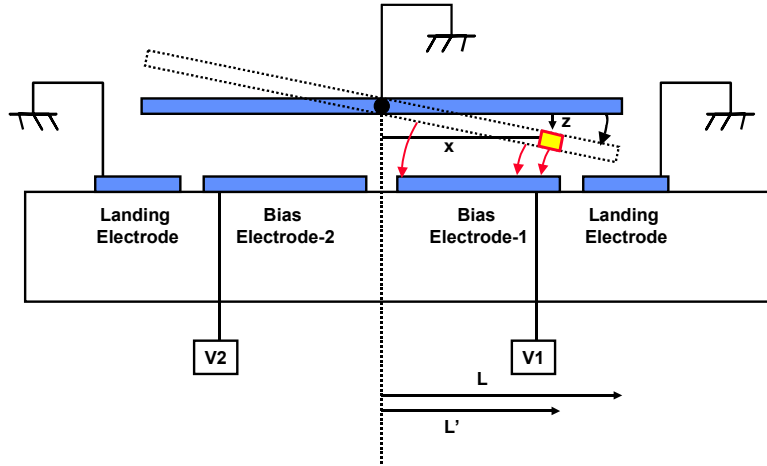


**EE M250B / MAE M282 / MBE M250B
HW#5 Solution**



Variable definition:

z_0 : initial gap

θ : rotation angle of mirror

θ_M : Maximum rotation angle (restrained by mechanical stopper)

w : mirror width

The mirror can be considered as many small parallel capacitors connected parallel
Force generated by the capacitor between the x and $x+dx$ equals to

$$dF = \left. \frac{\partial(dW * (V, g))}{\partial g} \right|_V = \frac{\epsilon V^2}{2g^2} w dx$$

Integrate dF from 0 to L' , we can get the total torque

$$\tau_a = \int_0^{L'} x \frac{\epsilon V^2}{2(z_0 - z)^2} w dx$$

Let $g = z_0 - z \quad \tan \theta = \frac{z}{x} \quad \tan \theta_M = \frac{z_0}{L}$

$$\tau_a = \frac{\epsilon V^2 W}{2} \int_0^{L'} \frac{x dx}{(z_0 - x \tan \theta)^2}$$

Use the technique of integration by parts. Let

$$u = x$$

$$du = dx$$

$$v = \frac{1}{\tan \theta (z_o - x \tan \theta)}$$

$$dv = \frac{x}{(z_o - x \tan \theta)^2}$$

$$\tau_a = \frac{\epsilon V^2 W}{2} \left\{ \left[\frac{x}{\tan \theta (z_o - x \tan \theta)} \right]_0^{L'} - \frac{1}{\tan \theta} \int_0^{L'} \frac{dx}{z_o - x \tan \theta} \right\}$$

$$\tau_a = \frac{\epsilon V^2 W}{2} \left\{ \left[\frac{x}{\tan \theta (z_o - x \tan \theta)} \right]_0^{L'} - \frac{1}{\tan \theta} \left[-\frac{1}{\tan \theta} \ln(z_o - x \tan \theta) \right]_0^{L'} \right\}$$

$$\tau_a = \frac{\epsilon V^2 W}{2 \tan \theta} \left[\frac{x}{z_o - x \tan \theta} + \frac{1}{\tan \theta} \ln(z_o - x \tan \theta) \right]_0^{L'}$$

$$\tau_a = \frac{\epsilon V^2 W}{2 \tan \theta} \left[\frac{L'}{z_o - L' \tan \theta} + \frac{1}{\tan \theta} \ln(z_o - L' \tan \theta) - \frac{1}{\tan \theta} \ln(z_o) \right]$$

$$\tau_a = \frac{\epsilon V^2 W}{2 \tan^2 \theta} \left[\ln \left(\frac{z_o - L' \tan \theta}{z_o} \right) + \frac{L' \tan \theta}{z_o - L' \tan \theta} \right]$$

$$\text{Let } z_o = L \tan \theta_M, \beta = \frac{L'}{L}$$

$$\tau_a = \frac{\epsilon V^2 W}{2 \tan^2 \theta} \left[\ln \left(\frac{L \tan \theta_M - \beta L \tan \theta}{L \tan \theta_M} \right) + \frac{\beta L \tan \theta}{L \tan \theta_M - \beta L \tan \theta} \right]$$

$$\tau_a = \frac{\epsilon V^2 W}{2 \tan^2 \theta} \left[\ln \left(1 - \frac{\beta \tan \theta}{\tan \theta_M} \right) + \frac{\beta \tan \theta}{\tan \theta_M - \beta \tan \theta} \right]$$

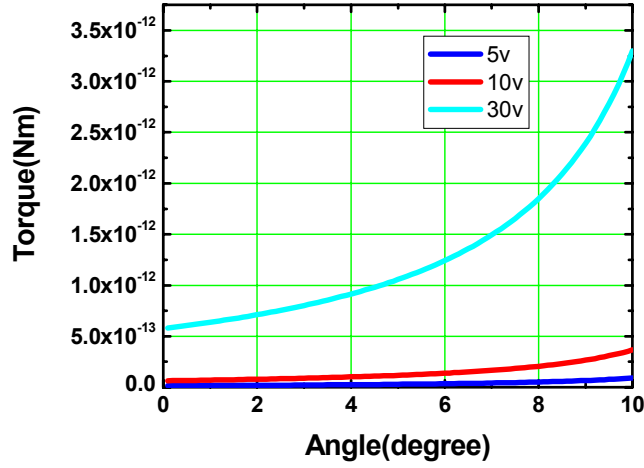
$$\text{Let } \alpha = \frac{\tan \theta}{\tan \theta_M}$$

$$\tau_a = \frac{\epsilon V^2 W}{2 \tan^2 \theta} \left[\ln(1 - \alpha \beta) + \frac{\alpha \beta \tan \theta}{\tan \theta - \alpha \beta \tan \theta} \right]$$

$$\tau_a = \frac{\epsilon V^2 W}{2 \tan^2 \theta} \left[\ln(1 - \alpha \beta) + \frac{\alpha \beta}{1 - \alpha \beta} \right]$$

$$\tau_a = \frac{\epsilon V^2}{2} \cdot \frac{W}{\tan^2 \theta_M} \left[\frac{1}{\alpha^2} \ln(1 - \alpha \beta) + \frac{\alpha \beta}{1 - \alpha \beta} \right]$$

(b)



(c) Compliance of the spring

$$C = \frac{1}{k}$$

$$k = \frac{KG}{L} \quad G = \frac{E}{2(1-\nu)} \quad K : ab^3 \left(\frac{16}{3} - 3.36 \frac{b}{a} \left(1 - \frac{b^4}{12a^4} \right) \right)$$

Where $a=0.5$ width=0.5 μ m , $b=0.5$ thickness=0.03 μ m , $E=70$ Gpa , $\nu=0.32$, $L=6$ μ m
Then

$$C = 1.68 \times 10^9 \text{ (rad/Nm)}$$

(d) Pull-in: When voltage above 212V, there is no intersection between the spring force and electrostatic force. Pull-in happens when under this condition.

